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The Common Myths about Control Systems Modelling

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Projects/stories in South Africa







IEEE TRANSACTIONS ON AUTOMATIC CONTROL, VOL. AC-13, NO. 3, JUNE 1968

Eigenvalue Sensitivity and State-Variable Selection

PATRICK E. MANTEY, MEMBER, IEEE

Manuscript received January 23, 1967; revised October 3, 1967, and February 12, 1968.

The author was with the Dept. of Electrical Engineering, Stanford University, Stanford, Calif. He is now with the IBM Research Lab., San Jose, Calif.



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Automatica, Vol. 5, pp. 85-93. Pergamon Press, 1969. Printed in Great Britain.

263

Selecting State Variables to Minimize Eigenvalue Sensitivity of Multivariable Systems*

R. A. SINGER†

* Manuscript received 10 July 1968 and in revised form 26 July 1968. Recommended for possible publication by associate editor P. Dorato.

† Ground Systems Group of Hughes Aircraft Company, Fullerton, California 92634, U.S.A., P.O.B. 3310.



Great minds on modeling



Our acceptance of models should thus be guided by 'usefulness' rather than 'truth.' - Lennart Ljung

Useful 益





1. Get the physics right

2. After that, it is all mathematics.

- Rudolf E Kalman



Make things as simple as possible, but not simpler.

- Albert Einstein

Simple 朴



All models are wrong, some are useful.

- George E P Box



Heavy haul trains modelling – the myth about state selection

2. HIV modelling – the myth about output selection

 Building energy maintenance modelling – the myth about input selection

4. Take home messages

1. Heavy haul trains modelling – the myth about state selection













Project definition

Problems



Objective of project

 The development of an applied software system for the control and handling of long trains (800 wagons, 10km long)

Industry partners

Spoornet

 Knorr-Bremse/New York Air Brake

EPC: EP-60 System Components



Independent distributed power (iDP)



Pneumatic control vs ECP

Pneumatic control



ECP



Model choice

Mass-point model

- Internal dynamics is ignored
- □ iDP control cannot be considered
- In-train forces is not investigated and thus the safe running can not be guaranteed



Model choice

Suspension model

$$\begin{split} m_{w}\ddot{y}_{w1} + \left(C_{py} + \frac{2f_{22}}{V_{s}}\right)\dot{y}_{w1} + K_{py}y_{w1} - 2f_{22}\psi_{w1} \\ -C_{py}\dot{y}_{b} - K_{py}y_{b} - C_{py}L_{b}\dot{\psi}_{b} - K_{py}L_{b}\psi_{b} = 0, \\ I_{w}\ddot{\psi}_{w1} + \frac{2f_{11}\lambda e}{r_{0}}y_{w1} + \left(\frac{2f_{11}e^{2}}{V_{s}} + C_{p\psi}\right)\dot{\psi}_{w1} \\ + K_{p\psi}\psi_{w1} - C_{p\psi}\dot{\psi}_{b} - K_{\psi b}\psi_{b} = T_{w1}, \\ m_{w}\dot{y}_{w2} + \left(C_{py} + \frac{2f_{22}}{V_{s}}\right)\dot{y}_{w2} + K_{py}y_{w2} - 2f_{22}\psi_{w2} \\ -C_{py}\dot{y}_{b} - K_{py}y_{b} + C_{py}L_{b}\dot{\psi}_{b} + K_{py}L_{b}\psi_{b} = 0, \\ I_{w}\ddot{\psi}_{w2} + \frac{2f_{11}\lambda e}{r_{0}}y_{w2} + \left(\frac{2f_{11}e^{2}}{V_{s}} + C_{p\psi}\right)\dot{\psi}_{w2} \\ + K_{p\psi}\psi_{w2} - C_{p\psi}\dot{\psi}_{b} - K_{p\psi}\psi_{b} = T_{w2}, \\ m_{b}\ddot{y}_{b} - C_{py}\dot{y}_{w1} - K_{py}y_{w1} - C_{py}\dot{y}_{w2} - K_{py}y_{w2} \\ + 2C_{py}\dot{y}_{b} + 2K_{py}y_{b} = 0, \\ I_{b}\ddot{\psi}_{b} - C_{py}L_{b}\dot{y}_{w1} - K_{py}L_{b}y_{w1} - C_{p\psi}\dot{\psi}_{w1} \\ -K_{p\psi}\psi_{w1} + C_{py}L_{b}\ddot{y}_{w2} + K_{py}L_{b}y_{w2} = 0 \end{split}$$



Model choice

Cascade-mass-point model

More accurate
Internal dynamics
In-train force
Full ECP/iDP



Longitudinal force model



Longitudinal dynamics model





Equations of motion

 $= 2, \cdots, n-1,$

$$m_{1}\ddot{x}_{1} = u_{1} - k_{1}(x_{1} - x_{2}) - d_{1}(\dot{x}_{1} - \dot{x}_{2}) - \underbrace{(c_{0} + c_{v}\dot{x}_{1})m_{1}}_{R^{r}}$$

$$- \underbrace{c_{a}\dot{x}_{1}^{2}\left(\sum_{i=1}^{n}m_{i}\right)}_{R_{a}} - 9.98\sin\theta_{1}m_{1} - 0.004D_{1}m_{1},$$

$$m_{i}\ddot{x}_{i} = u_{i} - k_{i}(x_{i} - x_{i+1}) - k_{i-1}(x_{i} - x_{i-1})$$

$$+ d_{i-1}(\dot{x}_{i-1} - \dot{x}_{i}) - d_{i}(\dot{x}_{i} - \dot{x}_{i+1})$$

$$- (c_{0} + c_{v}\dot{x}_{i})m_{i} - 9.98\sin\theta_{i}m_{i} - 0.004D_{i}m_{i}, i$$

$$m_n \ddot{x}_n = u_n - k_{n-1} (x_n - x_{n-1}) - d_{n-1} (\dot{x}_n - \dot{x}_{n-1}) - (c_0 + c_v \dot{x}_n) m_n - 9.98 \sin \theta_n m_n - 0.004 D_n m_n$$

State variable dimensions



Model validation

Trial on the 11th, 18th and 24th November 2003

- on the 11th: 4 locomotives—200 wagons—2 locomotives,
- on the 18th: 4 locomotives—100 wagons—2 locomotives—100 wagons,
- on the 24th: 6 locomotives—200 wagons.

GPS data

- Longitude and Latitude
- Track heights

GIS data

- Grade and curvature
- Other track characteristics



Validation: Trial run

Handwritten data:

- Current velocity
- Locomotive notch level
- Percentage brake applied

Electronically recorded data:

- Current velocity
- In-train force
- Brake pipe pressure









$$\begin{split} \mathsf{E} &= \sum_{i=1}^{n} \int \! u_i \, R_i u_i = \sum_{loco} \int \! u_i \, R_i u_i + \sum_{wagon} \int \! u_i \, R_i u_i \\ &= Loco \ \& \ Wagon \ Energy \ Consumption \\ &- Wagon \ Regenerative \ Energy \end{split}$$







Driver GUI







2. HIV modelling – the myth about output selection

Progression



HIVNET28: Vaccine Readiness

- Patients: 51 patients (10 Zimbabwean, 6 Malawian, 16 Zambian and 19 South African): 42 female, median age 28.
- Objective: set-point estimation



- average 8.9 months from seroconversion to first viral load measurement
- follow-up measurements at 2, 4, 7 and 9 months
- blood samples for plasma RNA levels, lymphocyte subset analysis and DNA isolation
- 34 with (5+4) measurements (viral load and CD4+)
- -10 with (4+4, 4+3) measurements
- 7 useless

Models 3D: biological backup and model

simplified HIV life-cycle

new virus particle buds from cell

new viral components congregate at cell surface

new viral RNA

new viral proteins



virus attaches to cell surface

virus core enters cell and its RNA is converted to DNA

cell nucleus

RNA copies are made which leave the nucleus

viral DNA enters nucleus and combines with host cell DNA

Russell Kightley Media, rkm.com.au

Models 3D: biological backup and model



Models 3D: reality reflection



$$P_{1} = \left(\frac{s}{d}, 0, 0\right);$$

$$P_{2} = \left(\frac{\mu_{1}\mu_{2}}{\beta k}, \frac{s}{\mu_{1}} - \frac{d\mu_{2}}{\beta k}, \frac{ks}{\mu_{1}\mu_{2}} - \frac{d}{\beta}\right);$$

$$R = \frac{\beta sk}{d\mu_{1}\mu_{2}}.$$

If R < 1, P_1 is stable Infection not spreading, vaccination

If R > 1, P_1 is unstable, P_2 is stable Infection spreading

Models 3D: the model is good (I)



Useful

- It simulates the stage from infection to clinic latency
- Set-point calculation is robust



Models 3D: the model is good (II)

Useful

益

• it simulates drug response

$$\frac{dT}{dt} = s - dT - \beta T v,$$
$$\frac{dT^*}{dt} = \beta T v - \mu_1 T^*,$$
$$\frac{dv}{dt} = kT^* - \mu_2 v.$$



The legendary

 Two Nature papers (Ho et al 95, Wei et al 95)

half life of virus = 6 hours (μ_2 = 3), half life of infected cells = 1 day (μ_1 = 0.45): rapid dynamics vs slow disease

- Citation over 500 within the year of publication
- Ho was elected the Man of the Year 1996, Time Magazine



Models 3D: the model is simple



Other models are more complex

Other Models: biological/immunological reasoning

- Burden theory
 - Explanation of CD4 depletion
- long-lived cell (4D)
 - Actively infected cells
 - Latently infected cells
- Multi-compartment theory: additional cellular reservoirs of virus (6D)
 - Follicular dendritic cells
 - Macrophage

Problems with current monitoring

- Measure anything
 - CD8+
 - actively infected CD4+
 - latently infected CD4+
- Measure anytime
 - in asymptomatic stage
- Measure many times
 - hundreds over 10 years
 - 16 in 8 days by Ho



Call for nonlinear identifiability theory

linear identifiability (well-known)

Tunali & Tarn (1987): first paper on nonlinear identifiability geometrical identifiability: one-one property of the i/o map w.r.t parameter

Diop (1991), Ljung & Glad (1994) and Glad (1997): algebraic and algorithmic — algebraic identifiability

Effects of initial conditions on identifiability noted in all papers, still under then current investigation in Denis-Vidal, Joly-Blanchard & Noiret (2001) and Saccomani, Audoly & Leontina (2003).
Nonlinear identifiability - concepts

Consider a nonlinear system,

$$\Sigma_{\theta} : \begin{cases} \dot{x} = f(x, \theta, u), x(0, \theta) = x_0 \\ y = h(x, \theta, u), \end{cases}$$

where $x \in \mathbb{R}^n, u \in \mathbb{R}^m$ and $y \in \mathbb{R}^p$ are the state, input and output variables of the system. Assume that

$$\operatorname{rank} \partial h(x,\theta,u)/\partial x = p.$$

 θ is the parameter to be identified.



I. INTRODUCTION

Definition 1 The system Σ_{θ} is said to be x_0 -identifiable at θ through an admissible input u (on [0, T]) if there exists an open set $\mathcal{P}^0 \subset \mathcal{P}$ containing θ such that for any two $\theta_1, \theta_2 \in \mathcal{P}^0, \theta_1 \neq \theta_2$, the solutions $x(t, \theta_1, x_0, u)$ and $x(t, \theta_2, x_0, u)$ exist on $[0, \epsilon]$, $0 < \epsilon \leq T$, and their corresponding outputs satisfy, on $t \in [0, \epsilon]$, $y(t, \theta_1, x_0, u) \neq t$ $y(t, \theta_2, x_0, u).$

Definition 2 The system Σ_{θ} is said to be structurally/geometrically identifiable if ...

Definition 3 The system Σ_{θ} is said to be algebraically identifiable if ...

Definition 4 The system Σ_{θ} is said to be identifiable with known initial conditions if

Nonlinear identifiability - algebraic framework

Let \mathcal{K} be the field consisting of meromorphic functions of x, θ, u and finite derivatives of u, and define

 $E = \operatorname{span}_{\mathcal{K}} \{ \mathrm{d}\mathcal{K} \},$

The vectors in *E* are called one-forms.

The differentiation of a function $\phi(x, \theta, u, ..., u^{(k)})$ along the dynamics of the system is defined as

$$\dot{\phi} = \frac{\partial \phi}{\partial x} f(x, \theta, u) + \sum_{i=0}^{k} \frac{\partial \phi}{\partial u^{(i)}} u^{(i+1)},$$

and this operation can be extended to differential one-forms $\omega = \kappa_x dx + \kappa_\theta d\theta + \sum \eta_i du^{(i)} \in E$ as the following:

$$\dot{\omega} = \dot{\kappa}_{x} dx + \dot{\kappa}_{\theta} d\theta + \sum \dot{\eta}_{i} du^{(i)} + \kappa_{x} df(x,\theta,u) + \sum \eta_{i} du^{(i+1)}.$$

Denote $\mathcal{Y} = \bigcup_{k=0}^{\infty} \operatorname{span}\{dy, d\dot{y}, \dots, dy^{(k)}\}, \mathcal{X} = \operatorname{span}\{dx\},$
$$\mathcal{U} = \bigcup_{k=0}^{\infty} \operatorname{span}\{du, d\dot{u}, \dots, du^{(k)}\}, \Theta = \operatorname{span}\{d\theta\}$$

Nonlinear identifiability - results

Theorem 1 The system is algebraically identifiable if and only if $\Theta \subset (\mathcal{Y} + \mathcal{U}).$

Theorem 2 The following statements are equivalent (1) The system Σ_{θ} is structurally identifiable; (2)

(3)

$$\Theta \subset \mathcal{X} + \mathcal{Y} + \mathcal{U},$$

$$\dim \frac{y + x + u}{x + u} = q.$$

(4) The system Σ_{θ} is identifiable with known initial conditions. **Theorem 3** (1) If

$$\mathcal{X} \cap (\mathcal{Y} + \Theta + \mathcal{U}) = \mathcal{X} \cap (\mathcal{Y} + \mathcal{U})$$
 (A)

then the system is algebraically identifiable if and only if it is structurally identifiable.

(2) If the system is algebraically identifiable, then (A) holds.

Nonlinear identifiability - algorithm 1

$$dy = \xi_1 dx + \gamma_1 d\theta \pmod{\mathcal{U}}$$

$$\vdots$$

$$dy^{(n-1)} = \xi_n dx + \gamma_n d\theta \pmod{\mathcal{U}}$$

One can also compute $dy^{(n)}$ as

$$dy^{(n)} = \xi_{n+1} dx + \gamma'_{n+1} d\theta \pmod{\mathcal{U}},$$
(B)

Due to observability, the matrix $[\xi_1^T, ..., \xi_n^T]^T$ is invertible, therefore dx can be written as a linear combination of dy, ..., dy⁽ⁿ⁻¹⁾ and d θ (mod \mathcal{U}). Substitution of dx in (B) yields the following expression of dy⁽ⁿ⁾: dy⁽ⁿ⁾ = $\sum_{i=1}^n \eta_i dy^{(i-1)} + \gamma_{n+1} d\theta$ (mod \mathcal{U}) More generally, one computes

$$dy^{(n+1)} = \sum_{i=1}^{n} \eta_{1i} dy^{(i-1)} + \gamma_{n+2} d\theta \pmod{\mathcal{U}}$$

:
$$dy^{(k^*)} = \sum_{i=1}^{n} \eta_{k^*-n,i} dy^{(i-1)} + \gamma_{k^*+1} d\theta \pmod{\mathcal{U}}$$

Nonlinear identifiability - algorithm 2

The system is geometrically identifiable if and only if there is a $k^* \ge q$ such that the matrix

$$\Gamma_g = \begin{bmatrix} \gamma_1 \\ \vdots \\ \gamma_k \end{bmatrix}$$

is of rank q.

The system is *algebraically identifiable* if and only if there is an $l^* \ge n + q$ such that the matrix

$$\Gamma_a = \begin{bmatrix} \gamma_{n+1} \\ \vdots \\ \gamma_{l^*} \end{bmatrix}$$

is of rank q.

Extension to: time-delay systems (Automatica02, TAC06) left Ore ring – non-commutative modules over the left Ore ring

3D model identifiability



Set-point estimation



- Mean estimates of parameter $=(7.48,0.00085,1.4 \times 10^{-6}, 1.56,0,80,2834)^{T}$
- Estimated set-point = $4.08 \log_{10} (12143 \text{ RNA copies/ml})$, time to set-point = 16.57 months
- (No difference with the European and US studies)

Dynamic HIV/AIDS Parameter Estimation With Application to a Vaccine Readiness Study in Southern Africa

R. A. Filter*, X. Xia, Senior Member, IEEE, and C. M. Gray

Abstract—This paper proposes a procedure of parameter esti-mation for all parameters of the three-dimensional HIV model. The least square based procedure uses standard optimization routines to allow parameter extraction for individual patients. It is shown how additional information from outside a measurement dataset can be included in the estimation routine to increase the reliability and accuracy of parameter estimates. A dataset from 44 patients of Southern Africa is analyzed to find the set point and the time until set point for these patients together with an estimate of the model parameters with confidence intervals for the cohort. The procedure is also applied to a long-term dataset of the HIV/AIDS progression to find possible variations in parameters

Index Terms-Bioengineering and medical systems, HIV/AIDS physical parameters, parameter estimation, parameter variation, set point estimation

I. INTRODUCTION

situations where it is not possible to extract all six, the procedure can accommodate generalizations of some parameters. This flexibility is achieved by implementing an estimation routine that combines standard optimization methods with a customizable least square (LSQ) based cost function.

IEEE TRANSACTIONS ON BIOMEDICAL ENGINEERING, VOL. 52, NO. 5, MAY 2005

The results are presented in three parts. First the basis of the estimation procedure is described. Secondly the procedure is validated with generated data and published parameter estimates. After validation, the estimation of viral set point and parameters for a cohort of patients from a HIV/AIDS vaccine readiness trial is presented. This is followed by an application where the procedure is applied to long-term data to extract possible variations of parameters. Finally conclusions from the results and impetus for further research are presented.

II. PROCEDURES

AIDS RESEARCH AND HUMAN RETROVIRUSES Volume 21, Number 4, 2005, pp. 285-291 @ Mary Ann Liebert, Inc

Short Communication

Viral Dynamics and CD4⁺ T Cell Counts in Subtype C Human Immunodeficiency Virus Type 1-Infected Individuals from Southern Africa

CLIVE M. GRAY,¹ CAROLYN WILLIAMSON,² HELBA BREDELL,³ ADRIAN PUREN,¹ XIAOHUA XIA,³ RUBEN FILTER,³ LYNN ZIJENAH,⁴ HUYEN CAO,⁵ LYNN MORRIS,¹ EFTHYIA MARK COLVIN,6 GLENDA GRAY,7 JAMES MCINTYRE,7 ROSEMARY MUSONDA,8 SUSAN ALLEN,8 DAVID KATZENSTEIN, MIKE MBIZO,4 NEWTON KUMWENDA,10 TAHA TAHA,10 SALIM ABDOOL KARIM.6 JORGE FLORES,11 and HAYNES W. SHEPPARD5

HIV / Nantes trial

Le traitement du sida amélioré grâce à des équations mathématiques

L'institut de recherche en communication et cybernétique de Nantes met au point une alde au diagnostic pour le traitemen du sida. Une étude a commencé en man sur un échantilion de patients.

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An example of a stratistic stratistratistic stratistic stratistic stratistic stratistic stratisti









Centre Universitaire Hospitalier de Nantes





Institut de Recherche en Communication et Cybernétique de Nantes

University of Pretoria

Goal and Protocol

Goal To predict the efficacy of a therapy To predict an immunologic or virologic failure.... Towards an early diagnosis...

Protocole

Initiation of a therapy for naiive patients3 blood tests during the 1st week2 blood tests during the 2nd week7 blood tests during the 1st month

11 blood tests for 3 months.....

Clinical data – patient 1





N	Date	t (Jours)	CD4 (CD4/mm ³)	CD8 (CD8/mm ³) CV (Copies/ml)		log10(CV)
1	14-Mar-2005	0	376	754	999833	6.00
2	15-Mar-2005	1	261	642	1309960	6.12
3	16-Mar-2005	2	422	788	442896	5.65
4	18-Mar-2005	4	524	1291	160130	5.20
5	25-Mar-2005	11	411	876	9684	3.99
6	4-Apr-2005	21	491	925	2956	3.47
7	11-Apr-2005	28	398	486	2297	3.36

Clinical data – patient 2





Ν	Date	t (Jours)	CD4 (CD4/mm ³)	CD8 (CD8/mm ³) CV (Copies/ml)		log10(CV)
1	14-Mar-2005	0	230	681	252013	5.40
2	15-Mar-2005	1	217	578	351121	5.55
3	16-Mar-2005	2	268	651	165919	5.22
4	18-Mar-2005	4	208	802	39214	4.59
5	25-Mar-2005	11	609	947	2966	3.47
6	1-Apr-2005	18	653	1151	1579	3.20
7	15-Apr-2005	32	547	1037	1534	3.19

Clinical data – patient 3





Ν	Date	t (Jours)	CD4 (CD4/mm ³)	CD8 (CD8/mm ³) CV (Copies/ml)		log10(CV)
1	22-Mar-2005	0	185	497	34423	4.54
2	23-Mar-2005	1	237	636	35199	4.55
3	24-Mar-2005	2	305	772	18490	4.27
4	29-Mar-2005	7	223	603	1541	3.19
5	4-Apr-2005	13	286	726	494	2.69
6	12-Apr-2005	21	181	379	170	2.23
7	21-Apr-2005	30	154	299	40	1.60

Results

	patient	S	δ	k	μ	s/δ
1	01	6.93	0.011	0.01	0.03	630
2	02	7.15	0.011	0.03	0.02	650
3	03	0.40	0.014	0.04	0.05	30
4	04	5.16	0.014	0.00	0.03	390
5	05	5.87	0.010	0.05	0.05	590
6	06	6.11	0.009	0.03	0.05	680

Immunologic failure



3. Building energy maintenance modelling – the myth about input selection

Control application in large scale lighting project



Funding Scheme Examples



United Nations Climate Change Carbon Mechanisms **CDM**: issue carbon emission reduction credits

- Large Scale
- Small Scale



Eskom: R 0.45 / kWh (R 0.55 for LED) savings for 3 years

- CFL Mass Rollout
- Performance Contracting
- Standard Offer



SANEDI: R 0.95 / kWh savings for 12 months

• 12 L Energy Efficiency Tax Incentive

Project Incentive Policy

- Project crediting period: 10 years
- PDs invest project implementation and maintenance
- PDs receive their rebate on annual basis
- PDs replace part/all of the failed EE lamps
- Savings reported by a third-party M&V inspection company
- Lamps maintained to ensure survival rate over 50%

Lighting Population Decay



Source: National Lighting Product Information Programme

Optimal Solutions (1)



Figure: Optimal control strategy of LED replacement.

Optimal Solutions (2)

Table: Key performance indicators with maintenance.

Key performance indicators	NM	FM	OM	OM vs. NM (%)	OM vs. FM (%)
Total investment	74.396	102.61	95.507	28	-7
Total profit	53.180	197.95	201.650	279	2
Cost–benefit ratio	0.7148	1.9293	2.1113	195	9
Energy saving	265,500	642,880	636,690	140	-1

NM, no maintenance; FM, full maintenance; OM, optimal maintenance; vs., versus.

[1] X. Ye and X. Xia, *in Proceedings of the 19th World Congress of the IFAC*, Cape Town, South Africa, August 24-29, 2014.
[2] X. Ye, X. Xia, L. Zhang, and B. Zhu, *Control Engineering Practice* 37(2015): 1–10.

Control System Inputs and Disturbances

* British Standard 3811 classified building maintenance as the followings:



Control System Inputs: *u_i*

Maintenance type

Corrective or preventive maintenance



Maintenance schedule

Periodically: weekly, monthly, annually Optimised: action on demand *or* event-triggered



Maintenance intensity

How many units to maintain

Control problems in BEE R&M - General Control System Framework

$$\begin{cases} \dot{x_i} = f_i(x, u) + d_i \\ y_j = h_j(x) + \omega_j \end{cases}$$

- *i*: grouping;
- $f_i(\cdot)$: control system **dynamics**;
- *u_i*: control system **inputs**;
- d_i: modelling errors;
- y_j: control system **outputs**;
- $h_j(\cdot)$: control system output function;
- *ω_j*: **measurement** errors and **sampling** errors.

(1)

BEE R&M: Failure Inspection and Modelling

Repairable

- Category: building envelopes, HVAC, water heaters
- Life span: long (> 10 years)

Non-repairable

- Category: lights, timers, switches, plug-device
- Life span: short (< 5 years)



Exponential Model: $f_i(x_i, u_i)$

J

Reparable failure modelling

Ref

$$x_i(k+1) = x_i(k)(1-\xi_i),$$

where $\xi_i = (\theta_i)^{-1}$, θ_i is the mean time between failure (MTBF).



B. Wang, X. Xia, and J. Zhang. *Energy and Buildings* 77 (2014): 227-235.
 EM Malatji, J. Zhang, and X. Xia. (2013). *Energy and Buildings*, 61(2013): 81-87.
 Y. Fan and X. Xia, An optimal maintenance plan for building envelope insulation materials after retrofitting, CAC 2015, 28 November 2015.

PELP Study: $f_i(x_i, u_i)$

Non-repairable failure modelling

$$x_i(k+1) = \frac{\tilde{b}_i \tilde{c}_i x_i(k)^2}{x_i(0)} - \tilde{b}_i x_i(k) + x_i(k) + u_i(k).$$



[1] H. Carstens, X. Xia, and X. Ye, *Applied Energy* 126(2014): 256 - 265.

Interactions (2): $f_i(x_i, u_i)$

Example 1

Interaction between lighting and HVAC $\begin{cases} \dot{x}_{Lamp} = \hat{f}_1(x_{Lamp}) + u_{Lamp}, \\ \dot{x}_{HVAC} = \hat{f}_2(x_{HVAC}, x_{Lamp}) + u_{HVAC}. \end{cases}$



Ref

Example 2

Interactions between retrofit and maintenance

$$\begin{cases} \dot{x}_{Retro} = \tilde{f}_1(x_{Retro}) + u_{Retro}, \\ \dot{x}_{Maint} = \tilde{f}_2(x_{Maint}, x_{Retro}) + u_{Maint} \end{cases}$$

 [1] B. Wang, N. Wang and X. Xia, Maintenance plan optimization with performance interplay in building energy efficiency retrofitting, CAC2015, 29 November 2015.
 [2] Z. Wu, B. Wang and X. Xia, Optimal planning of large-scale building energy efficiency retrofit, ICAE 2016, Beijing.

Multi-State: $f_i(x_i, u_i)$



$$\begin{cases} \Delta x_{l,M_{l}}(t_{k}) = -f_{M_{l},M_{l}-1}^{l} (x_{l,M_{l}}(t_{k})) - f_{M_{l},F}^{l} (x_{l,M_{l}}(t_{k})) + \sum_{i=1}^{M_{l}-1} u_{i}^{l}(t_{k}) + u_{c}^{l}(t_{k}) \\ \Delta x_{l,M_{l}-1}(t_{k}) = f_{M_{l},M_{l}-1}^{l} (x_{l,M_{l}}(t_{k})) - f_{M_{l}-1,M_{l}-2}^{l} (x_{l,M_{l}-1}(t_{k})) - f_{M_{l}-1,F}^{l} (x_{l,M_{l}-1}(t_{k})) - u_{M_{l}-1}^{l}(t_{k}) \\ \vdots \\ \Delta x_{l,2}(t_{k}) = f_{3,2}^{l} (x_{l,3}(t_{k})) - f_{2,1}^{l} (x_{l,2}(t_{k})) - f_{2,F}^{l} (x_{l,2}(t_{k})) - u_{2}^{l}(t_{k}) \\ \Delta x_{l,1}(t_{k}) = f_{2,1}^{l} (x_{l,2}(t_{k})) - f_{1,F}^{l} (x_{l,1}(t_{k})) - u_{1,M_{l}}^{l}(t_{k}) \end{cases}$$

B. Wang, Z. Wu, and X. Xia. *IEEE Transactions on Control Systems Technology*, vol. 25, no. 1, January 2017, pp. 374-381.

Optimal Maintenance Plan (1): u_i



[1] B. Wang, and X. Xia. The 19th IFAC World Congress, Cape Town, South Africa, 2014.
[2] B. Wang and X. Xia. Energy and Buildings 96 (2015): 299-308.

Optimal Maintenance Plan (1): u_i



Comparing with full maintenance strategy:

- Up to 30.7% of the maintenance cost is reduced,
- only 1.5% of the percentage energy saving is lost.

Optimal Maintenance Plan (2): u_i



B. Wang, Z. Wu, and X. Xia. IEEE Transactions on Control Systems Technology, vol. 25, no. 1, January 2017, pp. 374-381.

Optimal Maintenance Plan (3): u_i

Interactions between lighting and HVAC considered



B. Wang, N. Wang and X. Xia, Maintenance plan optimization with performance interplay in building energy efficiency retrofitting, CAC2015, 29 November 2015.

Optimal Maintenance Plan (4): u_i , Q_i



B. Wang, Z. Wu, B. Zhu and X. Xia. Optimal Control of Maintenance Instants and Intensities in Building Energy Efficiency Retrofitting Project. The 54th IEEE Conference on Decision and Control, Osaka, Japan, 2015.

Optimal Maintenance Plan (4): u_i , Q_i



Comparing with fixed-time-schedule:

- Up to 21.7% more energy saving, and
- up to 5.7% improvement on IRR.

Other issues

Outputs;

Objective functions;

Errors, disturbances and uncertainties;

Algorithms;

Groups.



4. Take home messages


... 复归于朴 朴散则为器 圣人用之 则为官长 故大制不割 ... 老子 (〈道德经〉28

"When Simplicity is broken up, It is made into instruments. Evolved individuals who employ them, Are made into leaders. In this way, the Great System is United." - Lao Tzu The Tao Te Ching (Verse 28)



并纪念高为炳教授!

对研究生博士学位论文和科学研究能力的情况介绍和综合评语: 十季以及+常同老经过医主教的考到 sh Ze 指导教师签名: 205 5(在 0月2日



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